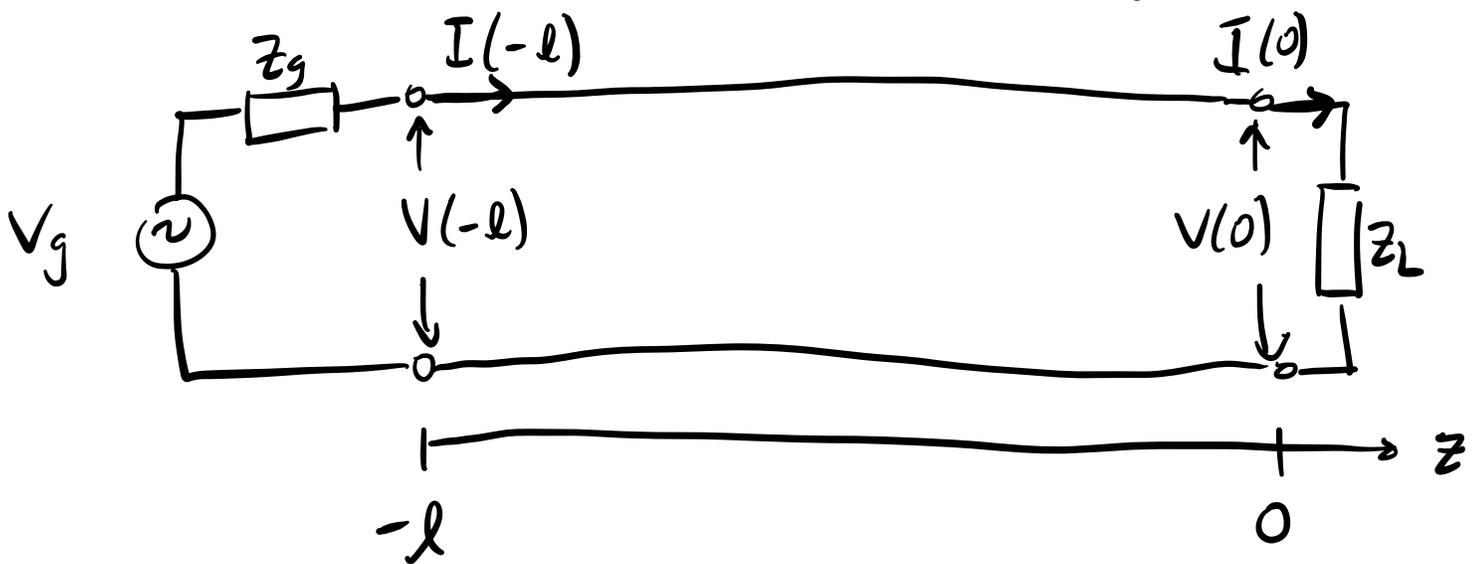


Useful results from earlier in the term:

1. Transmission line results for amplitude of harmonic voltage & current



Frequency Domain

$$\begin{cases} V(z, \omega) = V_+ [e^{-j\beta z} + \Gamma e^{j\beta z}] \equiv \hat{V}(z, \omega) \\ I(z, \omega) = \frac{V_+}{Z_0} [e^{-j\beta z} - \Gamma e^{j\beta z}] \equiv \hat{I}(z, \omega) \end{cases}$$

(Note: A blue circle with a '#' is around the first equation, and a red circle with an '*' is around the second equation.)

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0}$$

$$\beta = \omega \sqrt{L_l C_l} = \frac{\omega}{S}$$

prop. speed.

② Inverse Fourier Transforms

$$(a) f(t) = F^{-1}[\hat{f}(\omega)] = \frac{1}{2\pi} \int_{-\infty}^{\infty} \hat{f}(\omega) e^{j\omega t} d\omega$$

$$(b) \text{ Delta fun: } \delta(t-t_0) = \frac{1}{2\pi} \int_{-\infty}^{\infty} e^{j\omega(t-t_0)} d\omega$$

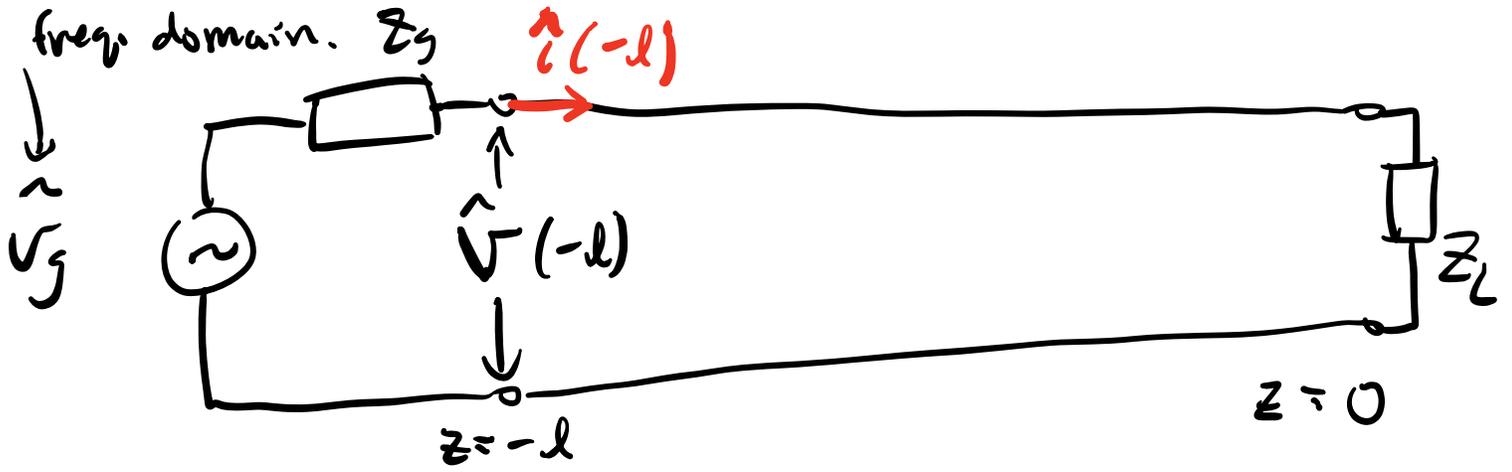
(c) Convolution Theorem

$$F^{-1}[\hat{x}_1(\omega) \hat{x}_2(\omega)] = x_1(t) * x_2(t) \\ = \int_{-\infty}^{\infty} x_1(\tau) x_2(t-\tau) d\tau$$

Goal is to calc. transient response (time domain) of a transmission line.

Strategy: Employ the freq. domain results that we already know.

Then take inverse Fourier transform to convert to time domain.



$\beta = \frac{\omega}{s}$

↑ speed

$$\hat{V}_g - \hat{i}(-l) Z_g = \hat{V}(-l) \quad \text{use } (*) \text{ for } \hat{i} \text{ w/ } z = -l$$

$$\hat{V}_g - \frac{V_+}{Z_0} \left[e^{j\omega l/s} - \Gamma e^{-j\omega l/s} \right] Z_g = \hat{V}(-l)$$

$$= V_+ \left[e^{j\omega l/s} + \Gamma e^{-j\omega l/s} \right] \quad \text{using } (\#)$$

~~Solve~~ Solve for V_+ (unknown)

$$V_+ = \frac{\hat{V}_g}{\left(e^{j\omega l/s} + \Gamma e^{-j\omega l/s} \right) + \frac{Z_g}{Z_0} \left(e^{j\omega l/s} - \Gamma e^{-j\omega l/s} \right)}$$

Assume that $Z_g = Z_0$ s.t. $\frac{Z_g}{Z_0} = 1$.

In this case,

$$V_+ = \frac{\hat{V}_g}{2} e^{-j\omega l/s}$$

For this special case, the volt. at the trans. line input in the freq. domain is $\hat{U}_{in} = \hat{U}(-l)$

$$\hat{U}_{in} = V_+ [e^{j\omega l/s} + \Gamma e^{-j\omega l/s}] \textcircled{\#}$$

$$= \frac{\hat{V}_g}{2} [1 + \Gamma e^{-2j\omega l/s}] \textcircled{!}$$

Suppose we meas. the volt. at trans. line input in the time domain using an osc. In that case, we expect to meas. the inverse Fourier trans. form of \hat{U}_{in} to get $U_{in}(t)$.

$$U_{in}(t) = F^{-1}[\hat{U}_{in}(\omega)] = F^{-1}\left[\frac{\hat{V}_g}{2} (1 + \Gamma e^{-2j\omega l/s})\right]$$

Let's assume that Γ is indep. of freq.

$$v_{in}(t) = \frac{1}{2} \underbrace{F^{-1}[\hat{V}_g]}_{V_g(t)} + \frac{\Gamma}{2} F^{-1} \left[\hat{V}_g \underbrace{e^{-2j\omega l/s}}_{\hat{x}_2(\omega)} \right]$$

$\hat{x}_1(\omega)$ $\hat{x}_2(\omega)$

apply convolution theorem.

$$F^{-1}[\hat{V}_g] * F^{-1}[e^{-2j\omega l/s}] \\ = V_g(t) * F^{-1}[e^{-2j\omega l/s}]$$

Note:

$$F^{-1}[e^{-2j\omega l/s}] = \frac{1}{2\pi} \int_{-\infty}^{\infty} e^{-2j\omega l/s} e^{j\omega t} d\omega$$

$$= \frac{1}{2\pi} \int_{-\infty}^{\infty} e^{j\omega(t - \underbrace{2l/s}_{t_0})} d\omega$$

$$= \delta(t - t_0) = \delta(t - 2l/s)$$

Note:

$$V_g(t) * F^{-1} \left[e^{-2j\omega l/s} \right]$$

$$= V_g(t) * \delta(t - 2l/s)$$

$$= \int_{-\infty}^{\infty} V_g(\tau) \delta[(t - 2l/s) - \tau] d\tau$$

Recall $\int f(t) \delta(t - t_0) dt = f(t_0)$

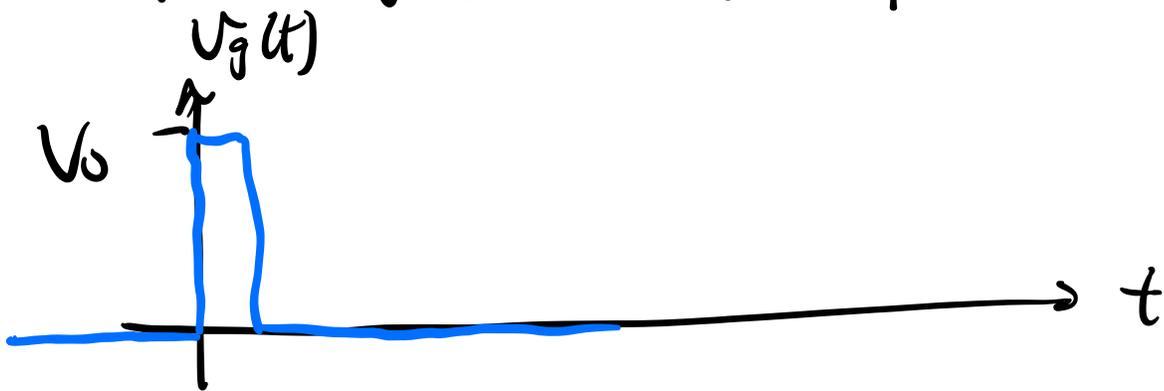
$$= V_g(t - 2l/s)$$

← represents
a delayed
pulse arriving
at input after
reflecting from end
of trans. line.

Bringing all of these results together:

$$V_{in}(t) = \frac{V_g(t)}{2} + \frac{\Gamma}{2} V_g(t - 2l/s)$$

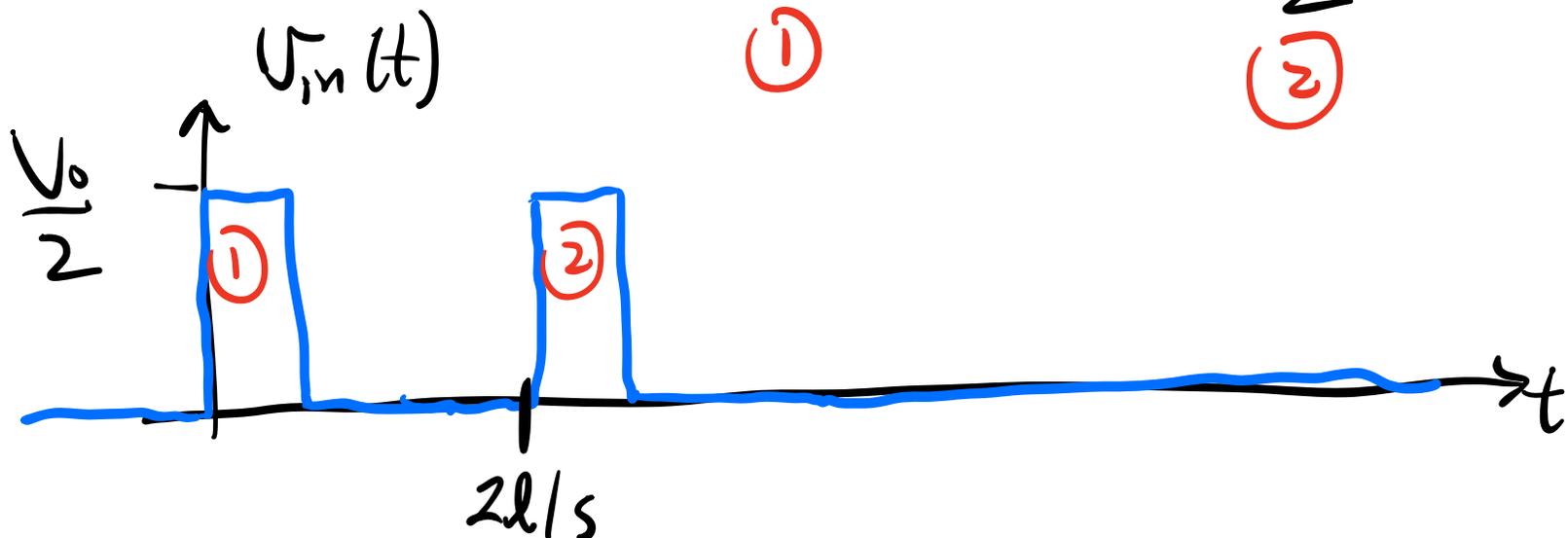
Suppose $V_g(t)$ is a square pulse



Case 1. $\Gamma = 1$ ($Z_L \rightarrow \infty$, open circuit)

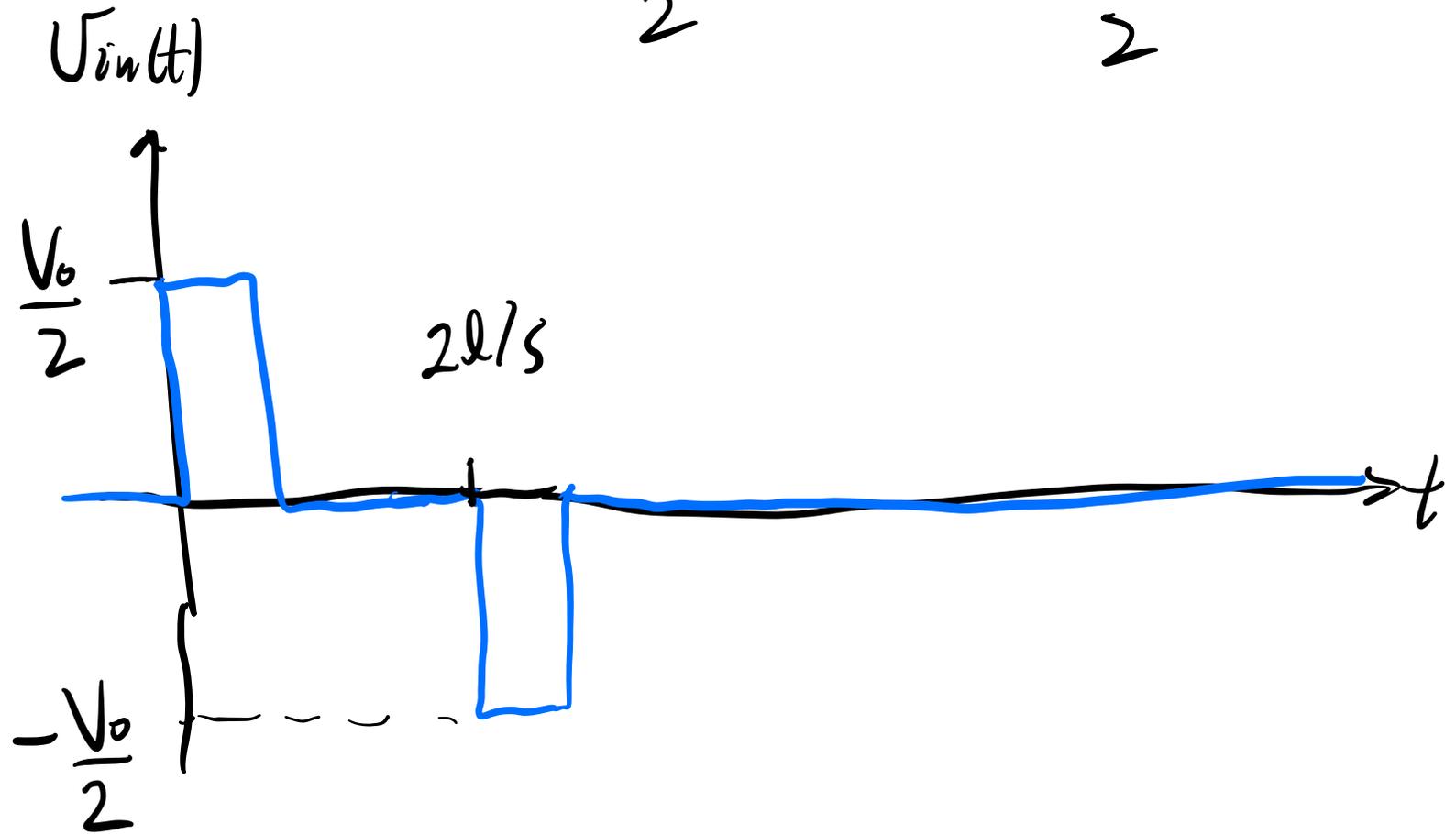
$$V_{in}(t) = \frac{V_g(t)}{2} + \frac{V_g(t - 2l/s)}{2}$$

① ②



Case 2. $\Gamma = -1$ ($Z_L = 0$, short circuit)

$$V_{in}(t) = \frac{V_g(t)}{2} - \frac{V_g(t - 2l/s)}{2}$$



Case 3. $\Gamma = 0$ ($Z_L = Z_0$)

$$V_{in}(t) = \frac{V_g(t)}{2}$$

